

QR and Mathematical Modeling

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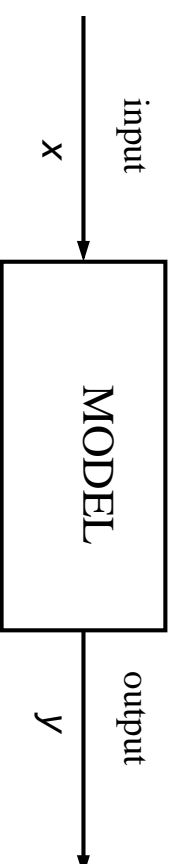
Outline

1. Introduction
2. Modelling from Data: System Identification (SI)
3. Problems in SI
4. What can **QR** do for **SI** ?
5. Brief overview of related work
6. *Part 1 - QR for structural (parametric) SI*
 - Case Study: Automated modeling system of visco-elastic materials and its application to pharmacology
7. *Part 2 - QR for black-box (non-parametric) SI*
 - Case Study: Kinetics of Thiamine (vitamin B_1) in the cells of the intestine tissue

Introduction

Quantitative mathematical model

A mathematical description of the relations between the inputs x (causes) and the outputs y (effects) of a system

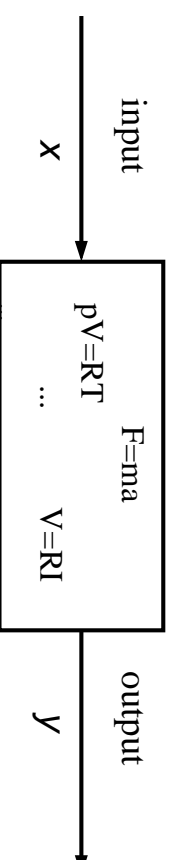


Model: a mapping $y = f(x)$

Three modeling approaches:

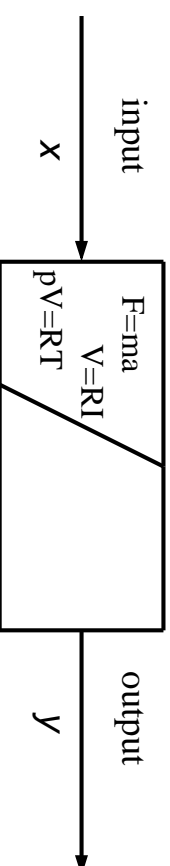
- white box
- grey box
- black box

White box modeling



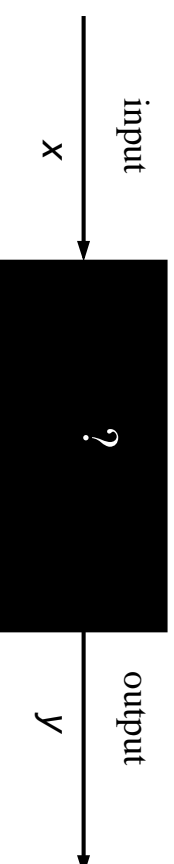
- Physical laws are available
- Typical examples: mechanical and electrical systems
- The box is “transparent”

Grey box modeling



- Physical laws are available but the values of some parameters are unknown
- the internal structure of the box is only partially known
- **Idea**: tune the unknown parameters until the outputs predicted by the model match the observed data

Black box modeling



- physical knowledge is not available
- physical knowledge is very incomplete
- parameter estimation is not possible due to the lack of adequate observed data sets
- useful for very complex systems
- **Idea**: collect data and use them to find the links between inputs and outputs

Problems in SI

- Choice of the **structural model** or **identifier scheme**
- appropriate set-up of numerical procedures
(e.g. initial conditions, start guess ...)
- Choice of adequate numerical methods
(e.g. curve fitting, ODE solvers,...)

What can QR do for SI ?

QR helps to:

- find model classes consistent with prior knowledge
- find an initial guess of parameter values
- choose proper numerical methods

Related work

- Kay [1996], Kay, Rinner, Kuipers [2000];
semi-quantitative SI
- Bradley [1994], Bradley, O’Gallagher, J. Rogers [1997];
M. Easley, E. Bradley [1999]
quantitative structural SI
- Capelo, Ironi, Tentoni [1996, 1998];
quantitative structural SI
- Bellazzi, Guglielmann, Ironi [1997, 1998, 2000];
quantitative “black-box” SI

Part 1

QR for structural SI

Case study: Automated modeling of
visco-elastic material

Structural modeling from data

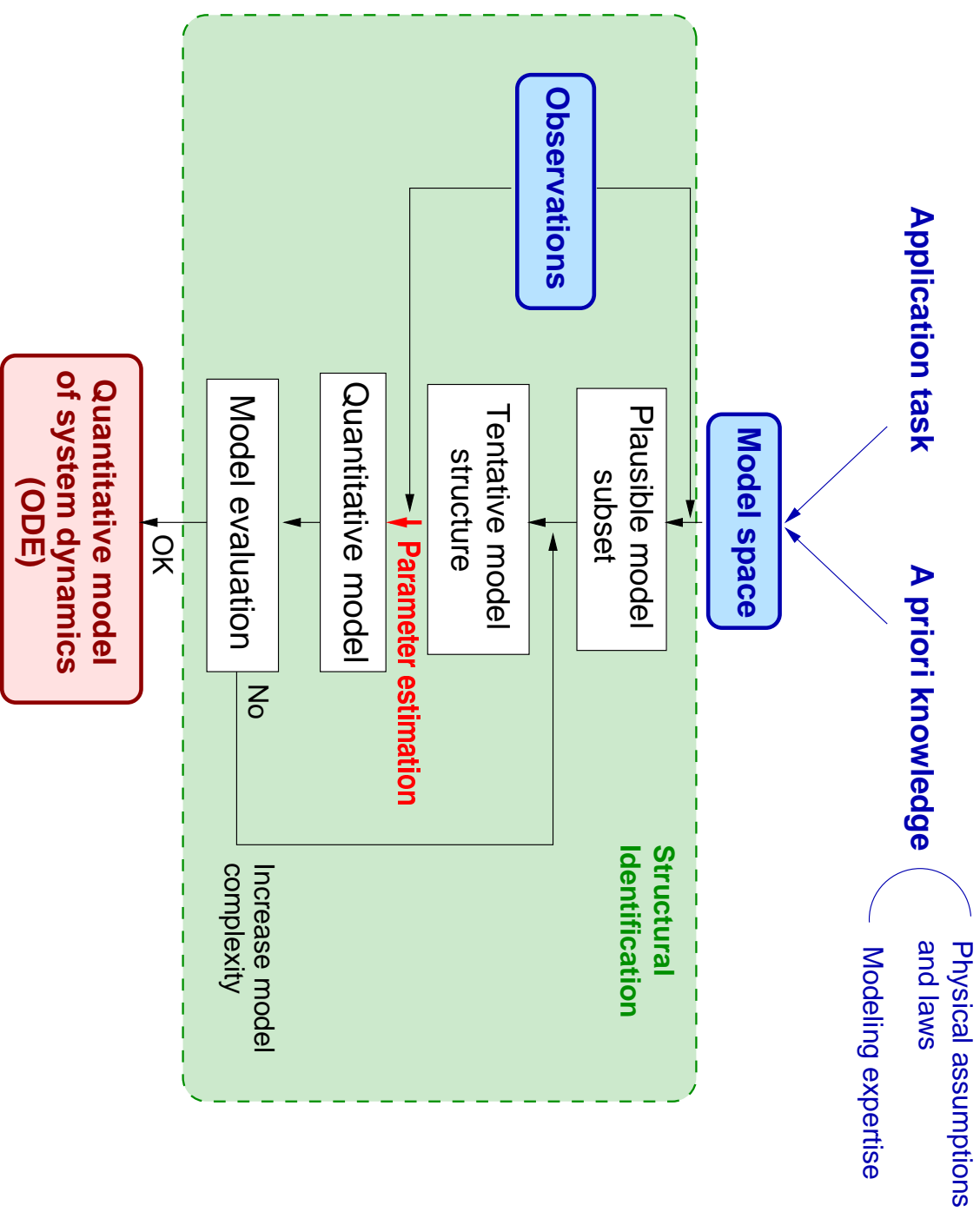
- Physical insight helps defining the **model space** (grey vs. black-box models)
- The model space definition requires modeling expertise

→ difficult task, not easily made automatic

System Identification: given the model space, the process of deriving a *good model* for the system dynamics from the observations

- SI grey modeling must not reduce to a mere numerical fit process
 - *adherence to the observations*
 - *minimal complexity*

System Identification

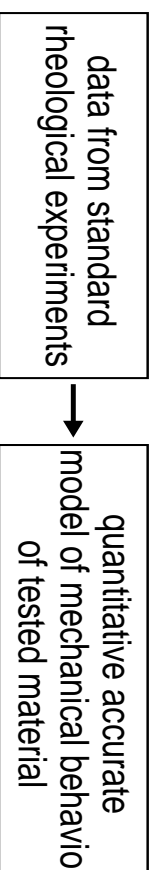


Use of QR in SI

- Intelligent data analysis
- Structural identification
- Parameter estimation

Automated modeling of visco-elastic materials

Motivations: assessment of visco-elastic materials from data



- deriving models by hand is a hard task
- models can be used for simulations, and provide a deeper insight w.r. to a mere experimental study

Goal: to formulate the constitutive equation $\mathcal{R}(s, e) = 0$ (linear ODE) describing the mechanical behavior of a material under suitable assumptions

Modeling issues

- **Modeling approach:** compositional strategy (rheology)
The model space was automatically generated, and partitioned into QB-homogeneous classes (see Capelo, Ironi, Tentoni 1998)

- **Experimental data:** Standard static tests - step input signal
 - Creep experiments: $s(t) \longrightarrow e(t)$
 - Relaxation experiments: $e(t) \longrightarrow s(t)$

Model space characterization (1)

The mathematical model describes the relation between $s(t)$ and $e(t)$:

$$\sum_i \theta_i^{(e)} D^i e = \sum_j \theta_j^{(s)} D^j s \quad \theta_i^{(e)}, \theta_j^{(s)} \in R$$

Formal model(FM):
symbolic ODE with the same ODE structure and $\theta_i \neq 0 \rightarrow 1$

The model space \mathcal{FM} can be partitioned as $\mathcal{FM} = \cup_{i=1}^4 \mathcal{FM}_i$,
and each class is associated with its own QB

Model space characterization (2)

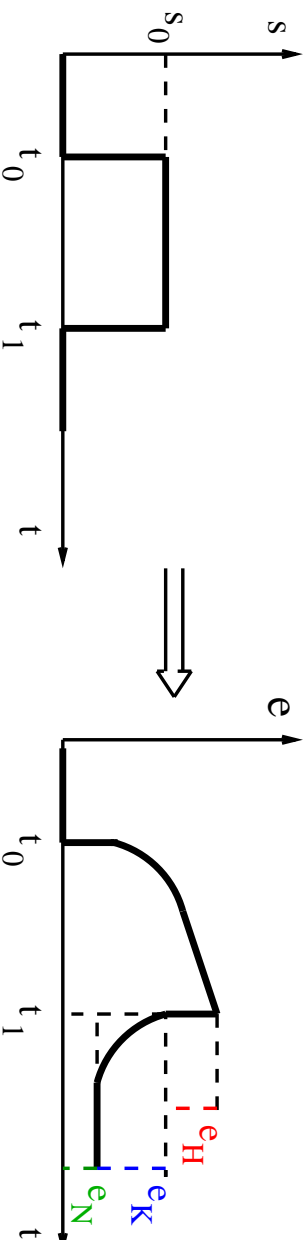
$$\mathcal{FM}_1 = \{FM_{1,k} : \sum_{i=0}^k D^i s = \sum_{i=0}^k D^i e, k \geq 0\} \leftrightarrow QB_1 = (T,T,F); (T,F,F)=QB(H)$$

$$\mathcal{FM}_2 = \{FM_{2,k} : \sum_{i=0}^k D^i s = \sum_{i=1}^{k+1} D^i e, k \geq 0\} \leftrightarrow QB_2 = (F,T,T); (F,F,T)=QB(N)$$

$$\mathcal{FM}_3 = \{FM_{3,k} : \sum_{i=0}^k D^i s = \sum_{i=0}^{k+1} D^i e, k \geq 0\} \leftrightarrow QB_3 = (F,T,F);$$

$$\mathcal{FM}_4 = \{FM_{4,k} : \sum_{i=0}^{k+1} D^i s = \sum_{i=1}^{k+1} D^i e, k \geq 0\} \leftrightarrow QB_4 = (T,T,T); (T,F,T)=QB(H-N)$$

Creep test

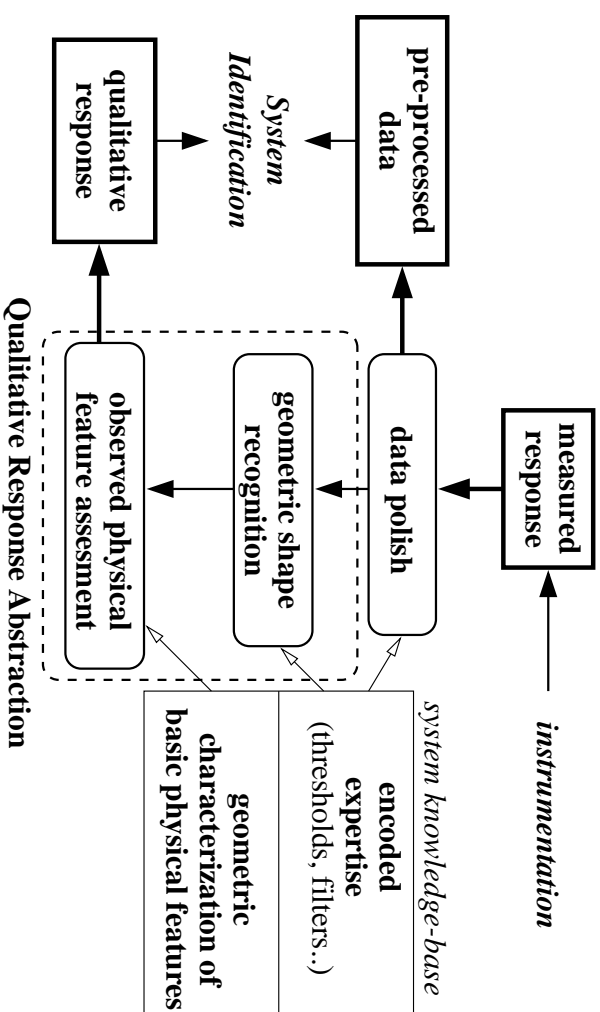


Qualitative strain response: $e = e_H + e_K + e_N$

$QB = (\alpha_H, \alpha_K, \alpha_N)$, where $\alpha_* = \text{True} \Leftrightarrow e_* \neq 0$

Intelligent Data Analysis

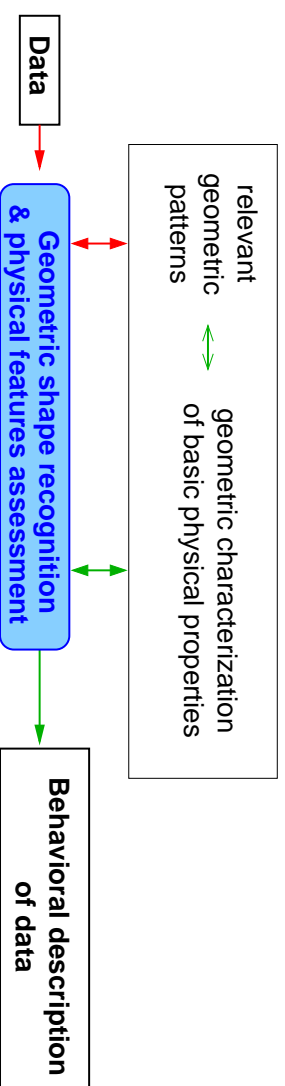
- Observations drive the whole modeling process



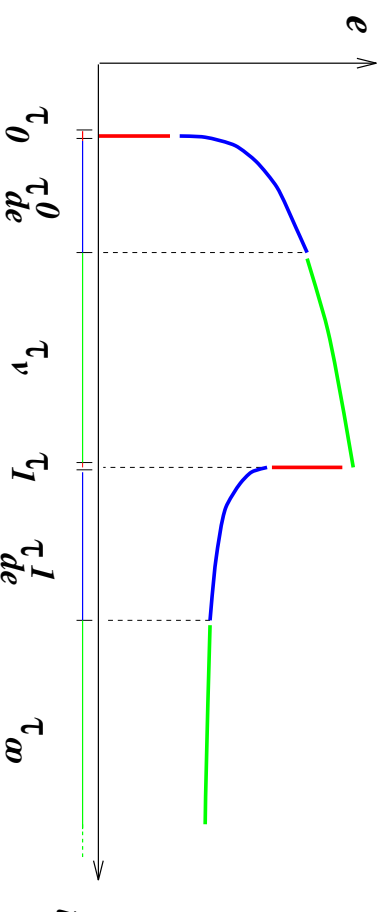
Data pre-processing

- removal of outliers
- filtering
- evaluation of measure uncertainty

Qualitative Response Abstraction



- **Geometric reasoning: shape recognition and data segmentation**



- **Inference of observed behavior from the extracted geometric features**

Structural Identification

Issue: select, within the model space, the subset of **plausible models**

→ more efficient computation
(reduced SI search space)

→ ensured physical accuracy

How:

DATA → QB_O → $\overline{\mathcal{FM}}$ | $QB_I = QB_O$

$\overline{\mathcal{FM}} \xrightarrow{FM^{-1}} \overline{\mathcal{M}} = \{M_k(\underline{\theta}), \underline{\theta} \in R^{N(k)} \setminus \{\underline{0}\}, k = 0, \dots, \bar{n}\}$

$$M_k(\underline{\theta}) : \sum_i \theta_i^{(e)} D^i e = \sum_j \theta_j^{(s)} D^j s$$

Quantitative Identification

The plausible model set $\overline{\mathcal{M}} = \{M_k(\underline{\theta})\}$ is hierarchical
(k : model complexity index, $\underline{\theta}$: model parameters)

Problem: Find k^* , $\underline{\theta}^*$ such that:

- $\underline{\theta}^* = \arg \min_{\theta} \sum_i^{N_D} \left(\frac{e(t_i; \underline{\theta}) - \bar{e}_i}{\sigma_i} \right)^2$
- and $\text{rcond}(\mathcal{F}) > 1.e - 5$, \mathcal{F} : information matrix
- $k^* = \arg \min_k AIC(k)$, AIC : Akaike Information Criterion

Properties of $M_{k^*}(\theta^*)$:

- numerical and statistical reliability
- minimal complexity
- reasonably good data fitting

Problems

- (P1) ◦ A *good* starting guess $\underline{\theta}^0$ must be provided
- (P2) ◦ Initial conditions $\mathbf{De}(t_0) = \mathbf{e}^0$ must be given
 - (De vector of the time derivatives of e)
 - ODEs $M_k(\underline{\theta})$ may be stiff

Problem ($\mathcal{P}1$)

A good guess θ^0 is needed to ensure convergence to the true (rather than to a local) minimum.

But θ^0 has no explicit physical meaning, and extracting information from data is not a straightforward task.

⇕

QR-driven curve fitting:

$$y(t; \mathbf{Q}, \mathbf{B}_O, \underline{\xi}, \underline{\lambda}) = \chi(\alpha_K) \cdot \sum_{i=1}^r c_i (1 - \exp(-\lambda_i t)) + \chi(\alpha_N) \cdot c_{r+1} t + \chi(\alpha_H) \cdot c_{r+2}$$

(exploits a priori knowledge and qualitative data interpretation)

+ *least-squares ODE collocation*: $\underline{\theta}^0$ l.s. solution of

$$\sum_i \theta_i^{(e)} D^i y(t_k) = \sum_j \theta_j^{(s)} D^j s(t_k) \quad , \quad (k = 1, \dots, N_D).$$

Problem ($\mathcal{P}2$)

- **Initial conditions e^0 must be given .**
 e_i^0 could be treated as further parameters to be identified as well, but this would entail a higher computational effort.



e^0 is defined by: $e^0 := \mathbf{D}y(t_0)$

- **$M_{r_k}(\underline{\theta})$ may be stiff, according to the elastic components of the response**
Explicit Adams or Runge-Kutta methods may be unstable



**Implicit, backward difference schemes (BDF, NDF) are preferred
(less accurate but stable)**

Remark: Stiff systems are frequent in many application domains: chemical kinetics, chemistry of polymers, mechanics...
A “stiff” system is characterized by time constants widely varying in magnitude.

Remarks

Traditional structural SI does benefit from the integration with QR

Integrated frameworks:

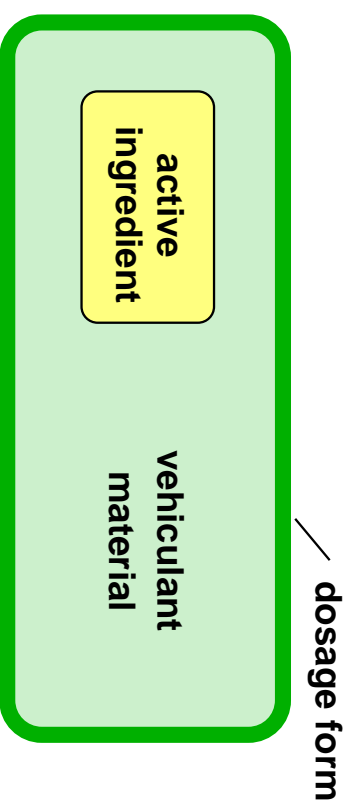
- allow us to deal automatically with modeling problems difficult to be handled by hand
- provide methodologies and tools for a deeper, more robust and economic investigation of physical domains traditionally studied at a mere experimental level

Application to Pharmacology

Motivations

Polymeric drug delivery research within the design of Drug Delivery Systems (DDS's)

DDS



Aim: ensuring optimal drug bioavailability (fast targeting + most effective delivery mode)

The development of a new DDS requires **assessment of those physicochemical properties of carrier materials** which affect bioavailability

Mucoadhesion

Mechanism whereby a polymeric carrier adheres to a mucosal tissue

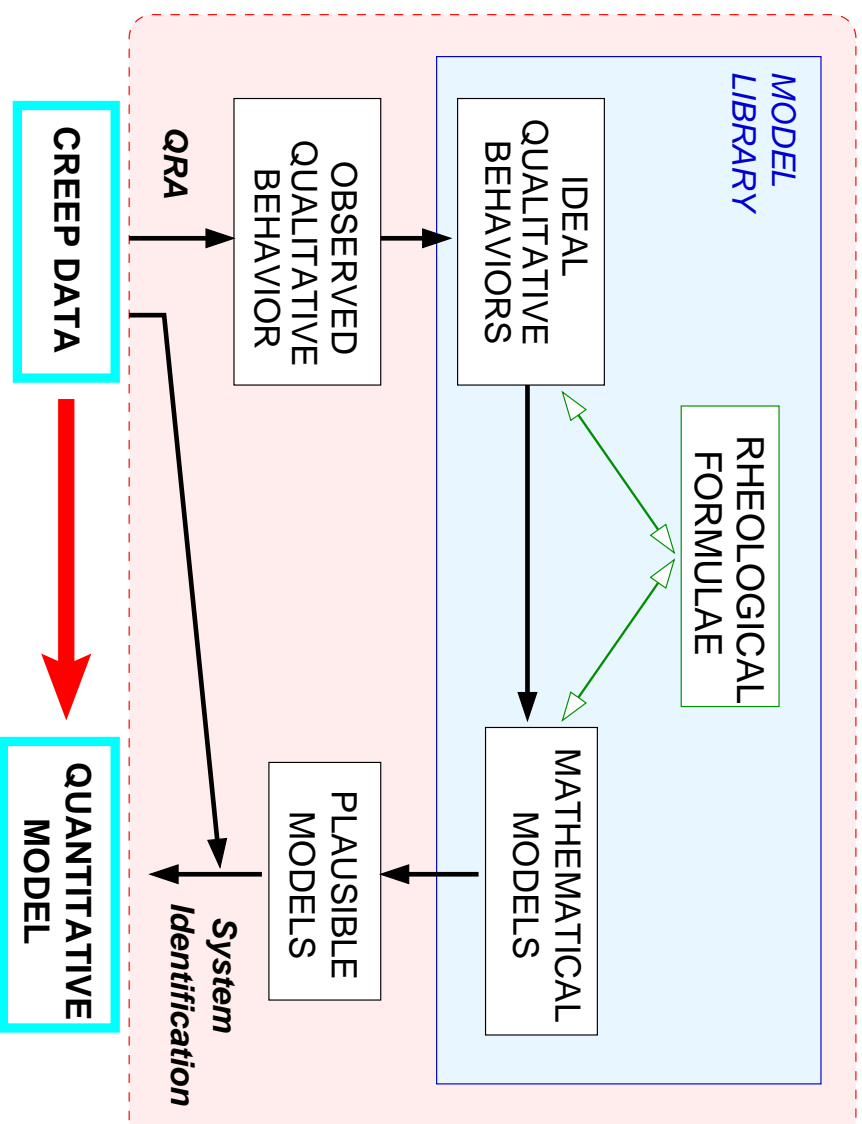
→ **A better mucoadhesive performance would improve drug bioavailability**

Traditional approach is entirely experimental:

- time consuming and costly
- it hardly provides info on the structural requirements for adhesion

A model based approach would provide a deeper comprehension of the polymer-mucus interaction

RHEOLO's architecture



Output: ODE model
compliance model

Résumé

Variables:

- $s(t)$ perturbation on the system (input)
- $e(t)$ elicited system response (output)

Data:

- Standard creep test: $s(t) = s_0 H(t - t_0)$

Models:

- ODE model
- Compliance model

Structural identification \rightarrow) class and order of the model

Parameter estimation \rightarrow values of the parameters

Compliance model

Explicitly related to the rheological structure of the material:

$$J(t) = J_0 + \sum_{i=1}^k J_i \left(1 - \exp\left(-\frac{t}{\tau_i}\right) \right) + \frac{t}{\eta_N}$$

$J_H(t) \leftrightarrow$ (instantaneous elasticity) J_0

Prompt elastic stretching of bonds between the primary structural units

$J_K(t) \leftrightarrow$ (retarded elasticity) $\{J_i, \tau_i\}_{i=1..k}$

Bonds break and reform, producing a slower, still recoverable, deformation.

$k \leftrightarrow$ number of bond types

$J_i \leftrightarrow$ intensity of each bond type

$\tau_i \leftrightarrow$ times at which the greater part of each bond type establishes

$J_N(t) \leftrightarrow$ (viscous flow) η_N

Irreversible rupture of bonds. In particular:

1. the # retardation times (model order), related to the establishment of new types of bonds, characterizes the material complexity
2. the compliance values express the strength of the structural units

The application problem

- **Materials**
 - **NaCMC**: solutions of polymer at three viscosity grades (LV, MV, HV), each one at three concentration levels (low, medium, high).
 - **Polymer+mucin**: mixtures of each polymer with mucin at three different concentrations

- **Aim**

Model-based investigation of polymer mucoadhesive performance, to get a deeper knowledge on the polymer-mucin interaction

Method

1. Quantitative characterization of rheological properties of each material by means of model order and parameters
2. Highlight structural conditions at which polymer-mucin synergy is higher (best mucoadhesive performance)

1 - Results

RHEOLOGICAL ANALYSIS TOOL-KIT

Model library generation | Data modelling | Q-Simulation | Quit

Qualitative data interpretation

Data file ==> bh16m8fn.csf

Dir | Data plot | Q-abstracton | Plausible models | Done

MATERIAL: BJanose High 1.6% + mucina 8% camp.

QUALITATIVE CURVE DESCRIPTION

CREEP: growing(t_0) concave(t_de_0) linear&growing(t_v)

ASSESSED QB: (F,T,T)

FEATURED PROPERTIES:
delayed elasticity
viscosity

Plausible models

Done

PLAUSIBLE MODEL CLASS \mathcal{E}_2 ($m = 1, 2, \dots, 9$)

- ODE :
$$\sum_{i=1}^{m+1} p_i \frac{d^i e}{dt^i} = \sum_{i=0}^m q_i \frac{d^i s}{dt^i}$$
- RF : $K_m - N$
- GSQM : $J(t) = \sum_{i=1}^m J_i (1 - \exp(-t/\tau_i)) + \frac{t}{\eta}$

Experimente

t_t_de

t_v

1 - Results

Model evaluation: Akaike indexes and condition numbers

k	Polymer (H.V. NaCMC 1.6%) + 8% mucin rcond	$A(k)$
0	1.00 e+00	1005.5
1	4.00 e-04	780.4
$k^* =$ 2	9.33 e-03	591.4
3	2.19 e-08	423.6

Optimal model order and parameter estimates (95% confidence intervals)

k^*	Polymer (H.V. NaCMC 1.6%) + 8% mucin	
k^*	2	
θ_1^*	1.568 e+2	[1.562 e+2, 1.574 e+2] Pa·s
θ_2^*	2.880 e+3	[2.879 e+3, 2.882 e+3] Pa·s ²
θ_3^*	8.128 e+2	[8.123 e+2, 8.132 e+2] Pa·s ³

2 - Results

		k^*
L.V. NaCMC low		0
Mixture with mucin		3
L.V. NaCMC medium		0
Mixture with mucin		2
H.V. NaCMC low		1
Mixture with mucin		2
H.V. NaCMC medium		2
Mixture with mucin		2

LV-NaCMC and HV-NaCMC at different concentrations, and their mixture with mucin at 8% concentration : optimal model order (k^*)

2 - Results

The addition of mucin causes an increase in the elastic properties, by the establishments of new bonds:

- increase in model order \leftrightarrow better interaction between polymer and mucin chains
- increase in the compliance values \leftrightarrow further strengthening of the mu-cohesive interface

The polymer-mucin interaction is highest when LV-NaCMC is used at the lowest concentration (deeper interpenetration)

Conclusive remarks

- RHEOLO has favoured a model based approach to the investigation of physicochemical properties relevant in DDS's design (e.g. mu-coadhesion)
- The proposed approach can be used to investigate phenomena involving variations in the material structure revealed by changes in the rheological behavior
- The model based approach has provided
 - deep insight into the polymer-mucin interactions
 - cheaper and more effective evaluation of polymer mucoadhesive performances through model parameters and complexity (rheological properties)

New application: Hemodynamics: study of blood rheological properties for diagnostic and therapeutic purposes

References

<http://ian.pv.cnr.it/~liliana/>

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